

Impact of Cattaneo-Christov heat flux on mixed convection flow of a ternary hybrid (Cu-Al₂O₃-TiO₂/H₂O) nanofluid over an elongated sheet: A comparative analysis

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The transfer of heat is an ineluctable part of science and engineering. The ternary hybrid nanofluid with its refined thermal properties exhibits superior heat transport capacity compared to hybrid nanofluids. Bearing in mind the extensive applications of this advanced fluid, the current research article deliberately investigates the impact of Cattaneo-Christov heat flux on the flow of a ternary hybrid nanofluid over an elongated sheet in the existence of thermal radiation. The proposed model is formulated by considering a base fluid of water dispersed with three distinct nanoparticles, Cu, Al₂O₃, and TiO₂. An application of the similarity transformation is made to change the controlling equations of the flow in dimensionless form. A numerical solution of the resulting equations is obtained by utilizing the bvp4c algorithm in MATLAB software. The results revealed that amplification in the values of the mixed convection parameter enhances the velocity profile of the ternary hybrid nanofluid and there is an advanced thermal transmission rate under the sway of Cattaneo-Christov thermal theory. It is further inferred from the current study that with varying volume fractions, trihybrid nanofluid demonstrates approximately 1.82-5.46% greater heat transfer than TiO₂/H₂O nanofluid and exhibits a stupendous thermal transmission rate over hybrid nanofluid and nanofluid.

Keywords: Cattaneo-Christov (C-C) thermal flux, Mixed convection, Stretching sheet, Ternary hybrid nanofluid, Thermal radiation

Introduction

Recent years have seen a significant increase in research on heat transfer up-gradation in industrial and production fields. This is attributed to the fact that the rate at which the heat is conducted determines the efficacy of most of the electronics, power generators, heat exchangers, etc. In order to acquire substantial enhancement in thermal transfusion rate, Choi and Eastman¹ proposed the notion of nanofluids, which are made by dispersing nanoparticles into conventional fluids. Nanofluids have proven to be beneficial in multiple fields of industrial and engineering applications, such as microelectronics, fuel chambers, pharmaceutical processes, nuclear reactors, and temperature reduction². Though the nanofluids seem to intensify the thermal conductivity (TC), industries need fluids which has a superior rate of heat transfer (RHT) compared with regular nanofluid. Hybrid nanofluids are fabricated by diffusion of two or more nanoparticles in the fluid base. As a result of their exceptional TC, hybrid

nanofluids have found numerous applications in various fields such as in tinning wires, space devices, crude oil extraction, welding, atomic reactors, the brake fluid of automobiles, etc. There are several factors contributing to the effective TC of hybrid nanofluids, such as how it is prepared, their size, shape factor, rate of dispersion of nanoparticles, surfactants, temperature, volume concentration, etc. By varying the temperature, Aparna *et al.*³ experimentally evaluated the TC of aqueous Al₂O₃-Ag/H₂O. As per the conclusion drawn from the study, a high temperature resulted in enlarged TC for the hybrid nanofluid. The leverage of nanoparticle size and structure on the hydrothermal behavior of plate evaporators by utilizing different hybrid combinations was explored by Bhattad and Sarkar⁴. They concluded that the functioning of the plate exchanger is robustly affected by the shape of the nanoparticles and the nanoparticles shaped like bricks are the most effective in heat transfer. Using GO-MoS₂/H₂O hybrid nanofluid, Kulkarni⁵ evaluated

the consequence of slip effect and thermal transfer features past a porous disk and inferred that the thermal transmission rate augments with enhancing nanoparticle sphericity.

Recent research about the nanofluids made by dispersion of three different nanoparticles has stimulated the inquisitiveness of researchers due to their strengthened heat transfer potentiality. This nanofluid, also known as tri-hybrid or ternary hybrid nanofluid, has an exceptional TC in comparison with regular and hybrid nanofluids. This was proved theoretically by Manjunatha *et al.*⁶ who considered the $Al_2O_3-TiO_2-SiO_2/H_2O$ trihybrid combination to ascertain the heat transmission features. Dezfulzadeh *et al.*⁷ investigated $Cu-SiO_2-MWCNT/H_2O$ ternary hybrid nanofluid with respect to its TC. In addition to evaluating its dynamic viscosity, they found the tri-hybrid nanofluid flaunts finer TC and enhanced viscosity over mono nanofluids and hybrid nanofluids. The ternary hybrid nanofluid $CuO-MgO-TiO_2/H_2O$ was explored by Mousavi *et al.*⁸ by varying the nanoparticle mixture ratio and temperature. They concluded that compared to purified H_2O , the tri-hybrid nanofluid in a combinative 60:30:10 ratio has the greatest TC which possessed an improvement by 78.6% for a volume fraction of 0.1% at 50°C. Their enriched heat transmission capability makes the THNF an ideal choice for applications in various sectors such as coolant in radiators⁹, in the photovoltaic thermal system¹⁰, evaporative coolers¹¹, etc. Few of the tectonic works done on heat transfer analysis involving ternary nanofluid can be referred¹²⁻¹⁶.

Combined forced and natural convection, also called mixed convection, is a mechanism in which both free and forced convection work together to transfer thermal energy. Mixed convection problems past a stretching sheet have captivated the interest of researchers over the past few decades. This is due to their broad list of applications in numerous fields such as nuclear reactors, electronics, petroleum reservoirs, chemical reactors, solar receivers, etc. El-Shorbagy *et al.*¹⁷ analyzed the mixed convective flow of Al_2O_3/H_2O nanofluid in a trapezoid shaped channel embedded in a porous media. They inspected the impact of thermal transfer on parameters such as Richardson number and Darcy number and concluded that a drop in the values of Richardson number accelerates the heat transfer rate, whereas heat

transfer is affected differently by Darcy number at every porous height. A numerical investigation on the mixed convection flow of Al_2O_3/H_2O nanofluid past a circular cylinder embedded in a porous media was studied by Al-Farhany and Abdulsahib¹⁸ and detected that elevating the values of Darcy number and volume fractions results in an increase in the values of Nusselt number. Waini *et al.*¹⁹ examined the steady mixed convective flow of Al_2O_3-Cu/H_2O hybrid nanofluid over an impermeable vertical surface and deduced that a decline in the mixed convective parameter degrades the velocity sketch of the hybrid nanofluid. There are also similar studies concerning free cum forced convection of hybrid nanofluid in²⁰⁻²⁵.

The transfer of energy(heat) as electromagnetic waves is referred to as “thermal radiation”. Radiative heat transfer in flow problems has profound impacts in the designing of propulsion devices, thermal systems, solar power plants, in the polymer industry, etc. The impact of radiation heat transfer in a natural convective flow of Al_2O_3/H_2O nanofluid within a diagonal rectangular enclosure was analyzed by Pordanjani *et al.*²⁶. Their study claimed that the rate at which the heat is transferred within the enclosure can be compounded by enhancing the values of radiation parameter. Reddy and Sreedevi²⁷ analyzed the contribution of thermal radiation to heat transmission characteristics of SWCNT/ H_2O nanofluid inside a square cavity and found that the heat transmission coefficient increases with accelerating values of the radiation parameter. A case study for estimating the thermal transport attributions of an unsteady MHD flow of a Casson nanofluid with the existence of radiation was carried out by Jamshed *et al.*²⁸. The sway of thermal radiation on the unsteady 2-D flow of MWCNT-Ag/ H_2O hybrid nanofluid along an elongated sheet was addressed by Sreedevi *et al.*²⁹. Escalation in temperature is observed with raising values of the radiation parameter and volume fraction of the nanoparticles. Wahid *et al.*³⁰ observed the same configuration of the temperature field in their investigation of the steady, mixed convective flow of a hybrid nanofluid over a flat vertical plate.

In general, heat transfer occurs when there exists a temperature gradient between two different materials or within the same one. The analysis of thermal transfer has been done by using Fourier’s law of heat conduction for centuries. But this classical law has the disadvantage that initial disruptions propagate

throughout the entire process. Cattaneo cleared this issue by fusing the term of thermal relaxation in Fourier's law. Later, Christov proposed a derivative law of Cattaneo, and the resulting thermal flux model is designated as the Cattaneo-Christov (C-C) thermal flux model. Based on the C-C thermal theory, Reddy *et al.*³¹ examined the thermal transport features of an MHD nanofluid flow passing through a whirling cylinder. Their study reported that the RHT strengthens with intensifying values of the thermal relaxation parameter. A comparative study between the thermal transport characteristics of distinct nanoparticles *Cu* and *CuO* in two distinct limitedly ionized fluids characterized by C-C theory was carried out by Abid *et al.*³². Considering the effect of thermal radiation and C-C heat flux, Azam³³ explored the two-dimensional magnetized flow of an incompressible Maxwell nanofluid. He noticed that boosting the magnetic parameter results in a declination of the RHT. The axisymmetric flow of *Cu - Al₂O₃ / H₂O* hybrid nanofluid past a stretching/shrinking sheet in a porous medium was investigated by Khan *et al.*³⁴. By employing C-C thermal flux, they developed a new iterative technique to find a numerical solution to the proposed model³⁵⁻⁴⁰ provides some recent descriptions of C-C thermal flux.

The ultimate intent of this study is to scrutinize the C-C influence on the mixed convective flow of a two-dimensional ternary hybrid nanofluid. An abundance of literature is available on a similar characterized flow of nanofluids and hybrid nanofluids, but no investigations have yet been conducted on ternary hybrid nanofluids. Thus, an attempt has been made to address this issue in this study. In this investigation, the following research inquiries are addressed:

- How does the presence of mixed convection influence the two-dimensional flow of ternary hybrid nanofluid over an elongated sheet?
- What is the consequence of C-C thermal theory on the thermal profile of the ternary hybrid nanofluid?
- Which type of nanofluid exhibits enhanced thermal transmission characteristics? Hybrid or Ternary?

Mathematical Formulation

The assumptions underlying fluid flow are as follows

1. Two-dimensional flow

2. Steady flow
3. Stretching sheet
4. Trihybrid nanofluid (*Cu - Al₂O₃ - TiO₂ / H₂O*)
5. Cattaneo-Christov heat flux
6. Incompressible ternary hybrid nanofluid

Thus, based on the assumptions outlined above, the flow of incompressible, trihybrid nanofluid past an elongated sheet has been considered in a steady, two-dimensional flow. In this model, $U_{\tilde{w}} = c\tilde{x}$ represents the velocity at which the sheet stretches. The configuration is portrayed through a rectangular coordinate system as shown in Fig. 1. The trihybrid nanofluid is created by suspending *Cu*, *Al₂O₃*, and *TiO₂* nanoparticles in water.

Given the aforesaid assumptions, the concerning PDE for the ternary nanofluid flow is modeled as follows³⁰

$$\frac{\partial \tilde{u}}{\partial \tilde{x}} + \frac{\partial \tilde{v}}{\partial \tilde{y}} = 0 \quad \dots (1)$$

$$\tilde{u} \frac{\partial \tilde{u}}{\partial \tilde{x}} + \tilde{v} \frac{\partial \tilde{u}}{\partial \tilde{y}} = \frac{\mu_{mf}}{\rho_{mf}} \frac{\partial^2 \tilde{u}}{\partial \tilde{y}^2} + g_r \frac{(\rho \beta_T)_{mf}}{\rho_{mf}} (\tilde{T} - \tilde{T}_\infty) \quad \dots (2)$$

$$\tilde{u} \frac{\partial \tilde{T}}{\partial \tilde{x}} + \tilde{v} \frac{\partial \tilde{T}}{\partial \tilde{y}} = \frac{k_{mf}}{(\rho c_p)_{mf}} \frac{\partial^2 \tilde{T}}{\partial \tilde{y}^2} + \frac{16\sigma^* \tilde{T}_\infty^3}{3k^*(\rho c_p)_{mf}} \frac{\partial^2 \tilde{T}}{\partial \tilde{y}^2} - \lambda_r \left\{ \left(\tilde{u} \frac{\partial \tilde{u}}{\partial \tilde{x}} + \tilde{v} \frac{\partial \tilde{u}}{\partial \tilde{y}} \right) \frac{\partial \tilde{T}}{\partial \tilde{x}} + \left(\tilde{u} \frac{\partial \tilde{v}}{\partial \tilde{x}} + \tilde{v} \frac{\partial \tilde{v}}{\partial \tilde{y}} \right) \frac{\partial \tilde{T}}{\partial \tilde{y}} + \tilde{u}^2 \frac{\partial^2 \tilde{T}}{\partial \tilde{x}^2} + \tilde{v}^2 \frac{\partial^2 \tilde{T}}{\partial \tilde{y}^2} + 2\tilde{u}\tilde{v} \frac{\partial^2 \tilde{T}}{\partial \tilde{x}\partial \tilde{y}} \right\} \quad \dots (3)$$

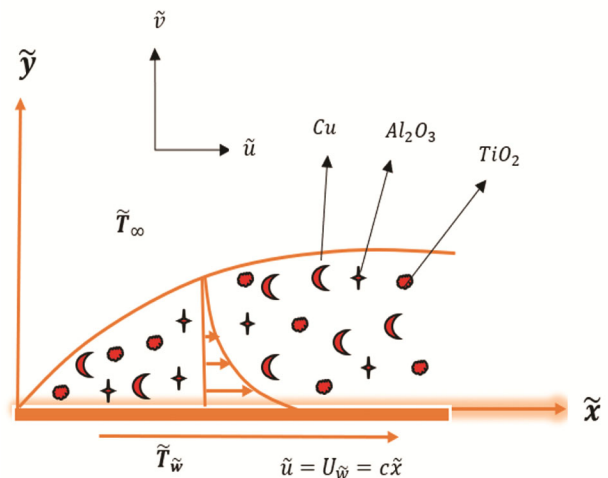


Fig. 1 — Configuration of the flow

Table 1 — Thermophysical characteristics of ternary hybrid nanofluid⁶

Thermo-physical Property	Ternary Hybrid Nanofluid
Dynamic Viscosity	$\mu_{mf} = \frac{\mu_f}{[(1-\phi_1)(1-\phi_2)(1-\phi_3)]^{10/4}}$
Density	$\frac{\rho_{mf}}{\rho_f} = (1-\phi_1) \left\{ (1-\phi_2) \left[(1-\phi_3) + \phi_3 \frac{\rho_3}{\rho_f} \right] + \phi_2 \frac{\rho_2}{\rho_f} \right\} + \phi_1 \frac{\rho_1}{\rho_f}$
Heat Capacity	$\frac{(\rho c_p)_{mf}}{(\rho c_p)_f} = (1-\phi_2) \left\{ (1-\phi_3) \left[(1-\phi_1) + \phi_1 \frac{(\rho c_p)_1}{(\rho c_p)_f} \right] + \phi_3 \frac{(\rho c_p)_3}{(\rho c_p)_f} \right\} + \phi_2 \frac{(\rho c_p)_2}{(\rho c_p)_f}$
Thermal expansion Coefficient	$\frac{(\rho \beta_T)_{mf}}{(\rho \beta_T)_f} = (1-\phi_2) \left\{ (1-\phi_3) \left[(1-\phi_1) + \phi_1 \frac{(\rho \beta_T)_1}{(\rho \beta_T)_f} \right] + \phi_3 \frac{(\rho \beta_T)_3}{(\rho \beta_T)_f} \right\} + \phi_2 \frac{(\rho \beta_T)_2}{(\rho \beta_T)_f}$
Thermal conductivity	$\frac{k_{mf}}{k_{hnf}} = \frac{k_1 + 2k_{hnf} - 2\phi_1(k_{hnf} - k_1)}{k_1 + 2k_{hnf} + \phi_1(k_{hnf} - k_1)}$ Where $\frac{k_{mf}}{k_f} = \frac{k_2 + 2k_{nf} - 2\phi_2(k_{nf} - k_2)}{k_2 + 2k_{nf} + \phi_2(k_{nf} - k_2)}$ and $\frac{k_{mf}}{k_f} = \frac{k_3 + 2k_f - 2\phi_3(k_f - k_3)}{k_3 + 2k_f + \phi_3(k_f - k_3)}$

with the boundary constraints⁴³

$$\tilde{u} = U_{\tilde{w}} = c\tilde{x}; \quad \tilde{v} = 0; \quad \tilde{T} = \tilde{T}_{\tilde{w}}; \quad \text{at } \tilde{y} = 0$$

$$\tilde{u} \rightarrow 0; \quad \tilde{T} \rightarrow \tilde{T}_{\infty}; \quad \text{as } \tilde{y} \rightarrow \infty \quad \dots (4)$$

The thermophysical characteristics and the numerical values for density, thermal expansion coefficient, thermal conductivity, and heat capacity associated with Cu , Al_2O_3 , and TiO_2 nanoparticles and H_2O are illustrated in Tables 1 and 2.

Following are the similarity variables utilized to non-dimensionalize the PDEs mentioned above^{6,35,41}

$$\psi = \tilde{x} \sqrt{c\nu_f} f(\eta); \quad \tilde{u} = \frac{\partial \psi}{\partial \tilde{y}}; \quad \tilde{v} = -\frac{\partial \psi}{\partial \tilde{x}}; \quad \theta(\eta) = \frac{\tilde{T} - \tilde{T}_{\infty}}{\tilde{T}_{\tilde{w}} - \tilde{T}_{\infty}}; \quad \eta = \sqrt{\frac{c}{\nu_f}} \tilde{y} \quad \dots (5)$$

The equation of continuity (1) is identically gratified and (2)-(4) takes on the following form

$$g''' - N_1 N_2 (g'^2 - gg'') + N_1 N_3 \lambda \theta = 0 \quad \dots (6)$$

$$N_3 \theta'' + Rd \theta' + N_4 Pr g \theta' - \delta_e N_4 Pr (gg' \theta' + g^2 \theta'') = 0 \quad \dots (7)$$

Table 2 — Numerical values of thermal conductivity, thermal expansion coefficient, heat capacity, and density of the nanoparticles and the base fluid^{15,24}

Thermophysical Characteristics	Cu	Al_2O_3	TiO_2	H_2O
$k (Wm^{-1}K^{-1})$	400	40	8.9538	0.613
$\beta \times 10^{-5} (K^{-1})$	1.67	0.85	0.9	21
$c_p (J/kgK)$	385	765	686	4179
$\rho (kgm^{-3})$	8933	3970	4250	997.1

$$\text{At } \eta = 0, \quad g = 0, \quad g' = 1, \quad \theta = 1$$

... (8)

$$\text{As } \eta \rightarrow \infty, \quad g' \rightarrow 0, \quad \theta \rightarrow 0$$

$$\text{Where } \lambda = \frac{Gr_{\tilde{x}}}{Re_{\tilde{x}}^2}; \quad Gr_{\tilde{x}} = \frac{g_r (\beta_T)_f (\tilde{T}_{\tilde{w}} - \tilde{T}_{\infty}) \tilde{x}^3}{\nu_f^2}; \quad Re_{\tilde{x}} = \frac{\tilde{x} U_{\tilde{w}}}{\nu_f};$$

$$Rd = \frac{16 \sigma^* \tilde{T}_{\infty}^3}{3 k^* k_f}; \quad Pr = \frac{\nu_f}{\alpha_f}; \quad \delta_e = c \lambda_{\tau} \quad \text{are the non-}$$

dimensional parameters involved in (6)-(7). Also, it should be noted that $\lambda > 0$ indicates aiding flow, $\lambda < 0$ represents impeding flow and $\lambda = 0$ signifies forced convection flow. N_1 , N_2 , N_3 , N_4 and N_5 are described by,

$$N_1 = [(1 - \phi_1)(1 - \phi_2)(1 - \phi_3)]^{10/4}$$

$$N_2 = (1 - \phi_1) \left((1 - \phi_2) \left[1 - \phi_3 + \phi_3 \frac{\rho_3}{\rho_f} \right] + \phi_2 \frac{\rho_2}{\rho_f} \right) + \phi_1 \frac{\rho_1}{\rho_f}$$

$$N_3 = (1 - \phi_1) \left((1 - \phi_2) \left[1 - \phi_3 + \phi_3 \frac{(\rho\beta_T)_3}{(\rho\beta_T)_f} \right] + \phi_2 \frac{(\rho\beta_T)_2}{(\rho\beta_T)_f} \right) + \phi_1 \frac{(\rho\beta_T)_1}{(\rho\beta_T)_f}$$

$$N_4 = (1 - \phi_1) \left((1 - \phi_2) \left[1 - \phi_3 + \phi_3 \frac{(\rho c_p)_3}{(\rho c_p)_f} \right] + \phi_2 \frac{(\rho c_p)_2}{(\rho c_p)_f} \right) + \phi_1 \frac{(\rho c_p)_1}{(\rho c_p)_f}$$

$$N_5 = \frac{k_{mf}}{k_f} = \left(\frac{k_1 + 2k_{mf} - 2\phi_1(k_{mf} - k_1)}{k_1 + 2k_{mf} + \phi_1(k_{mf} - k_1)} \right)$$

$$\left(\frac{k_2 + 2k_{mf} - 2\phi_2(k_{mf} - k_2)}{k_2 + 2k_{mf} + \phi_2(k_{mf} - k_2)} \right)$$

$$\left(\frac{k_3 + 2k_f - 2\phi_3(k_f - k_3)}{k_3 + 2k_f + \phi_3(k_f - k_3)} \right)$$

The dimensional form of the engineering quantities of interest, skin friction coefficient ($C_{f\bar{x}}$), and Nusselt number ($Nu_{\bar{x}}$) is given by⁴³

$$C_{f\bar{x}} = \frac{\tau_w |_{\tilde{y}=0}}{\rho_f (\tilde{U}_w)^2} \text{ and } Nu_{\bar{x}} = \frac{\tilde{x}q_w |_{\tilde{y}=0}}{k_f (\tilde{T}_w - \tilde{T}_\infty)} \quad \dots (9)$$

In which $\tau_w = \mu_{mf} \frac{\partial \tilde{u}}{\partial \tilde{y}}$ describes the shear stress

and $q_w = -k_{mf} \frac{\partial \tilde{T}}{\partial \tilde{y}} - \frac{16 \sigma^* \tilde{T}_\infty^3}{3 k^*} \frac{\partial \tilde{T}}{\partial \tilde{y}}$ is the heat flux.

(9) takes the following dimensionless form by making use of the similarity transformation (5),

$$C_{f\bar{x}} \text{Re}_{\bar{x}}^{1/2} = \frac{1}{N_1} f''(0), \quad Nu_{\bar{x}} \text{Re}_{\bar{x}}^{-1/2} = -(N_5 + Rd) \theta'(0) \quad \dots (10)$$

Numerical Solution

The system of non-linear differential equations (6)-(7) is initially transformed into a system of first order ODEs by implementing the following procedure.

$$g = m_1, \quad g' = m_2, \quad g'' = m_3, \quad \theta = m_4, \quad \theta' = m_5, \quad \dots (11)$$

Invoking (11) in (6) and (7), we obtain,

$$m_3' = g''' = N_1 N_2 (m_2^2 - m_1 m_3) - N_1 N_3 \lambda m_4$$

$$m_5' = \theta'' = \frac{1}{(N_5 + Rd - m_1^2 \delta_e N_4 \text{Pr})}$$

$$[\delta_e N_4 \text{Pr} m_1 m_2 m_5 - N_4 \text{Pr} m_1 m_5]$$

The corresponding transmuted boundary conditions are,

$$m_1 = 0, \quad m_2 = 1, \quad m_4 = 1, \quad \text{at } \eta = 0$$

$$m_2 \rightarrow 0, \quad m_4 \rightarrow 0 \quad \text{as } \eta \rightarrow \infty$$

The remodelled ODEs are evaluated numerically with the bvp4c function in MATLAB software. Depending on the values of the parameters that were used, we selected $\eta \rightarrow \infty$ values to be 5 (i.e.) $\eta_\infty = 5$.

Results and Discussion

A graphical interpretation of the effects of numerous dimensionless, pertinent parameters on the ternary hybrid nanofluid flow profiles is discussed in the current section. These parameters include mixed convection parameter λ , Prandtl number Pr , thermal relaxation parameter δ_e , radiation parameter Rd , and volume fraction ϕ . Here, ϕ_1, ϕ_2, ϕ_3 respectively denotes the volume fraction of Cu , Al_2O_3 , and TiO_2 nanoparticles. The established Prandtl number for water is approximately 6.9 and hence our investigation strategically encompasses a range of Prandtl numbers, specifically targeting values between 6 and 6.9 ($6.0 \leq \text{Pr} \leq 6.9$). Since the Brinkman viscosity model has been employed, the volume fraction of nanoparticles has been constrained to be less than 4% ($0.01 \leq \phi < 0.04$). The mixed convection parameter is deliberately set between -1 and 2 to examine the effects of assisting, opposing, and forced convective flows on the flow profiles ($-1 \leq \lambda \leq 2$). Also, the thermal relaxation parameter and radiation parameter are set within the range ($0.01 \leq \delta_e \leq 0.2$) and ($0.1 \leq Rd \leq 2.5$) following^{32,29,41}.

Scrutinization of velocity field

Influence of buoyancy parameter on the velocity field for Cu/H_2O nanofluid, $Cu-Al_2O_3/H_2O$ hybrid nanofluid and $Cu-Al_2O_3-TiO_2/H_2O$ ternary hybrid nanofluid is presented in Fig. 2. Accelerating the buoyancy parameter results in an enhancement of the velocity profile. Mixed convection, in general, is described by the buoyancy force versus the inertial force ratio. As λ enhances, the influence of buoyancy forces becomes dominant

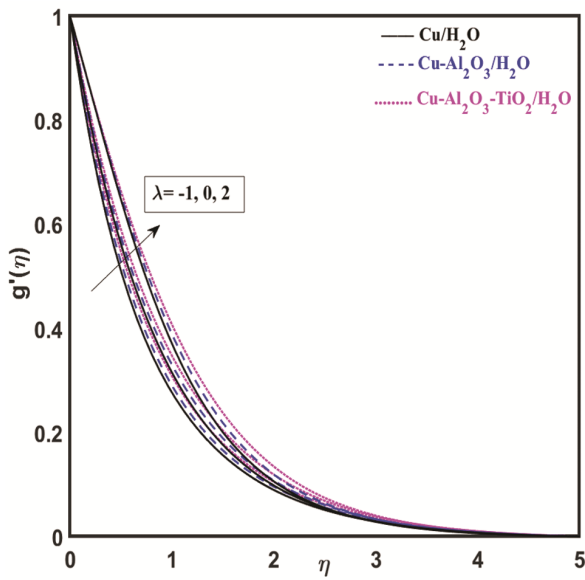


Fig. 2 — Implication of λ on $g'(\eta)$

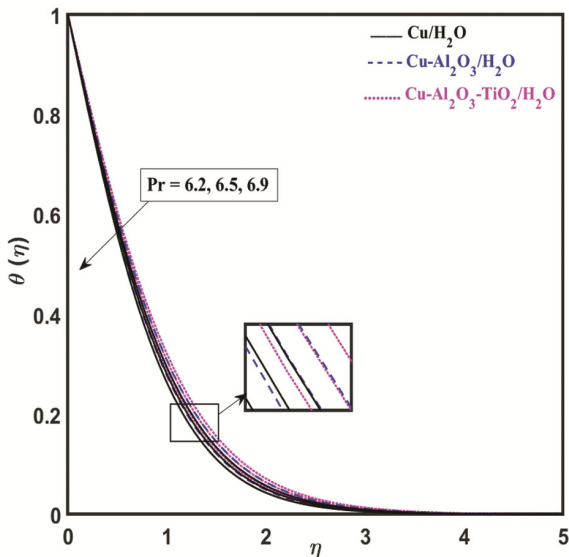


Fig. 3 — Implication of Pr on $\theta(\eta)$

over the inertial forces, thereby boosting the velocity.

Scrutinization of temperature field

Fig. 3 depicts the variation in temperature against different values of Pr for Cu/H_2O nanofluid, $Cu-Al_2O_3/H_2O$ hybrid nanofluid and $Cu-Al_2O_3-TiO_2/H_2O$ ternary hybrid nanofluid. It is observed that maximizing the Pr values decline the thermal profile. The Prandtl number relates inversely to heat diffusivity by definition. An augmentation in the Pr values diminishes the heat diffusion rate and hence the temperature of the liquid reduces. A demonstration of how the thermal field is affected by radiation parameter Rd is portrayed in Fig. 4. A rise in temperature is perceived with expanding values of radiation parameter Rd . Fig. 5 represents the sway of thermal relaxation parameter δ_e on the thermal gradient for Cu/H_2O nanofluid, $Cu-Al_2O_3/H_2O$ hybrid and $Cu-Al_2O_3-TiO_2/H_2O$ tri-hybrid nanofluid. Accelerating the δ_e values constrict the temperature sketch of nanofluid, hybrid and ternary hybrid nanofluid. The conductive behavior of the fluid particles decreases with proliferating δ_e values, thus leading to a depletion in temperature.

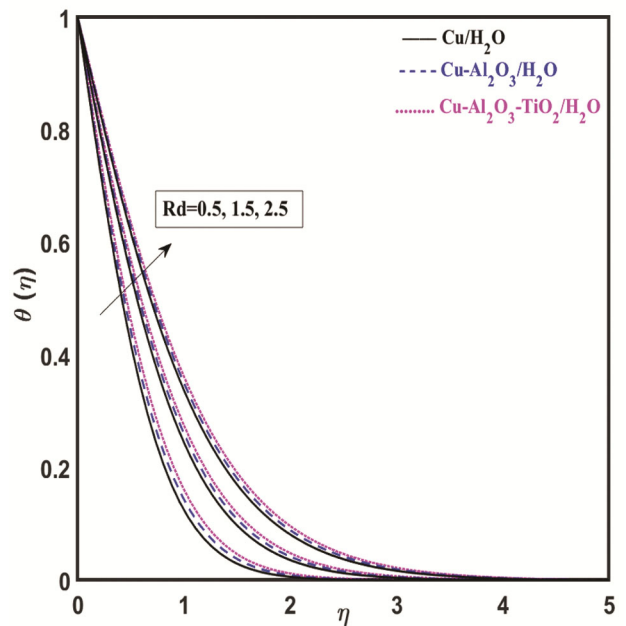


Fig. 4 — Implication of Rd on $\theta(\eta)$

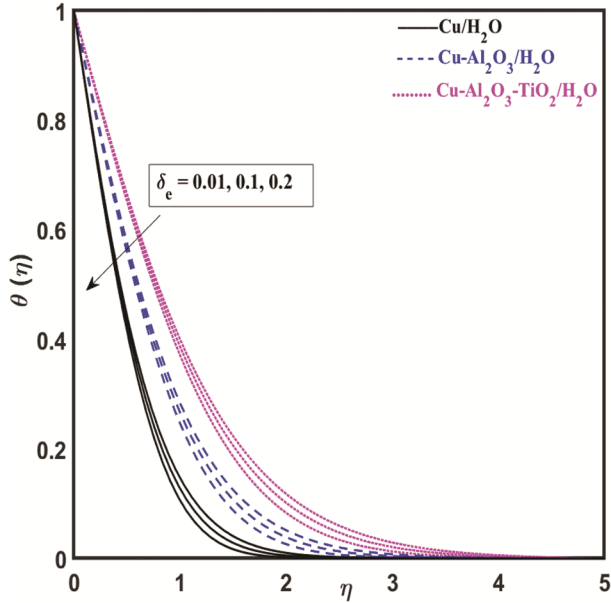


Fig. 5 — Implication of δ_e on $\theta(\eta)$

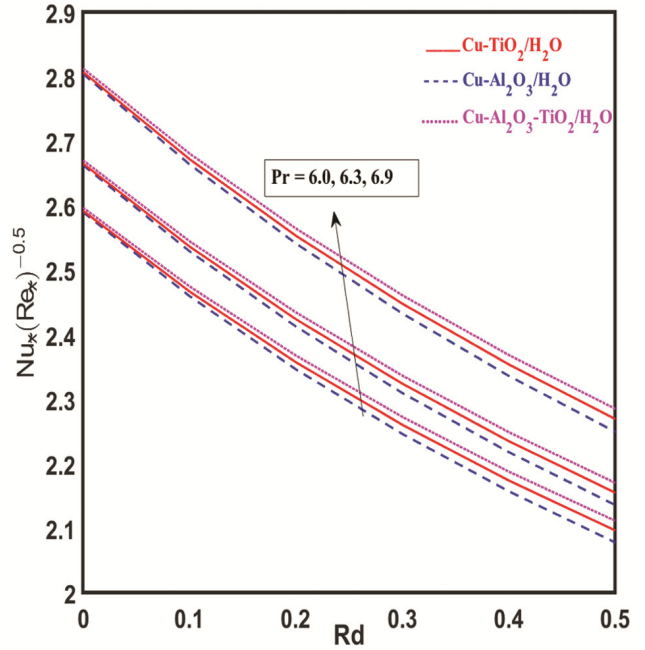


Fig. 7 — Implication of Pr and Rd on $Nu_x(Re_x)^{-0.5}$

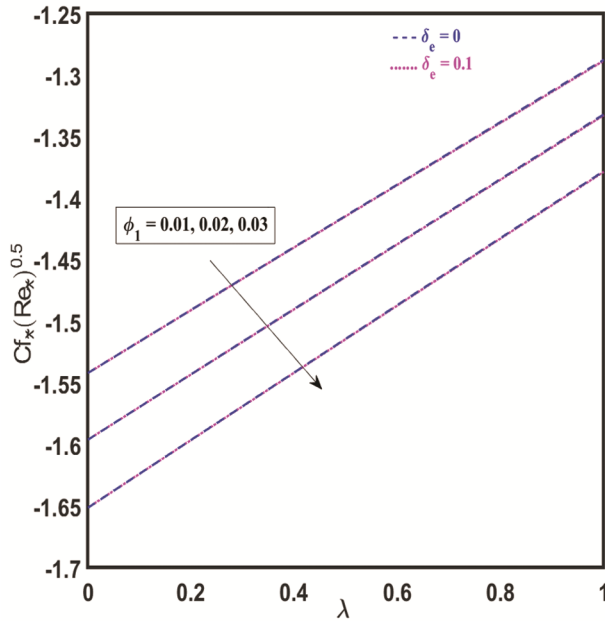


Fig. 6 — Implication of ϕ_1 and λ on $Cf_x(Re_x)^{0.5}$

Scrutinization of engineering quantities of interest

Fig. 6 illustrates the discrepancy in the values of skin-friction coefficient against λ for distinct values of ϕ_1 . It can be inferred from the figure that the graph of $Cf_x(Re_x)^{0.5}$ gets compressed with an enhancement in the values of ϕ_1 but intensifies through λ . Also,

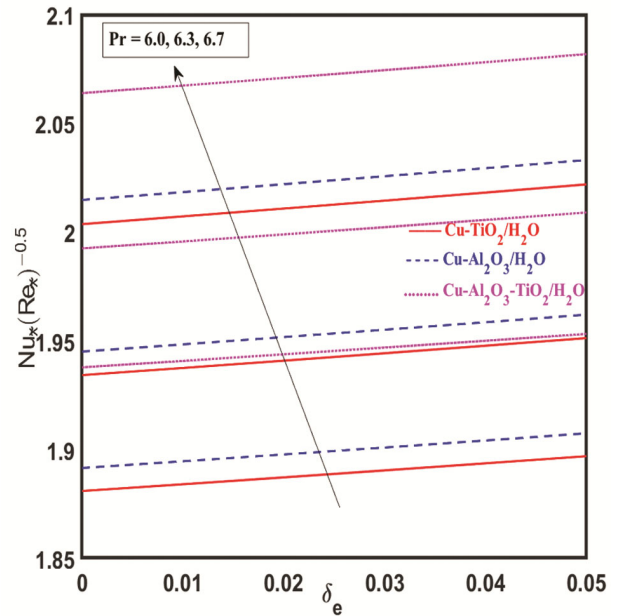


Fig. 8 — Implication of Pr and δ_e on $Nu_x(Re_x)^{-0.5}$

the values of the drag force seem to be dominating in the absence of δ_e rather than in the presence of it. The RHT, which is calculated by using Nusselt number, are portrayed in Fig. 7 and 8. According to Fig. 7, the values of $Nu_x(Re_x)^{-0.5}$ increases with Pr

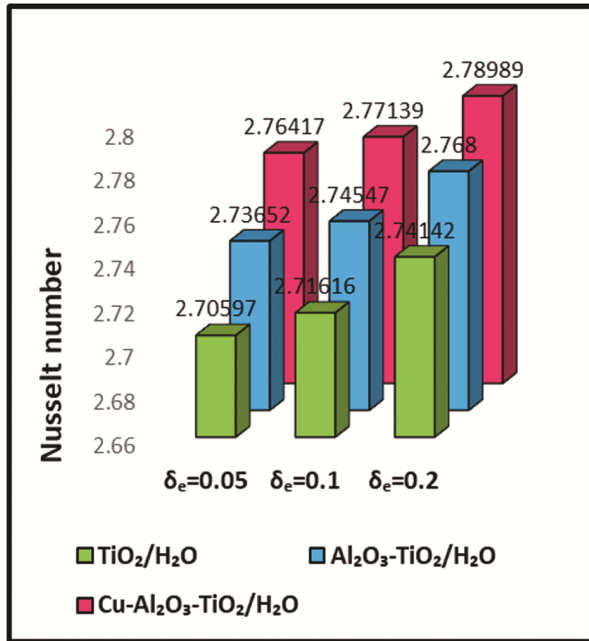


Fig. 9 — Discrepancy in Nusselt number against δ_e

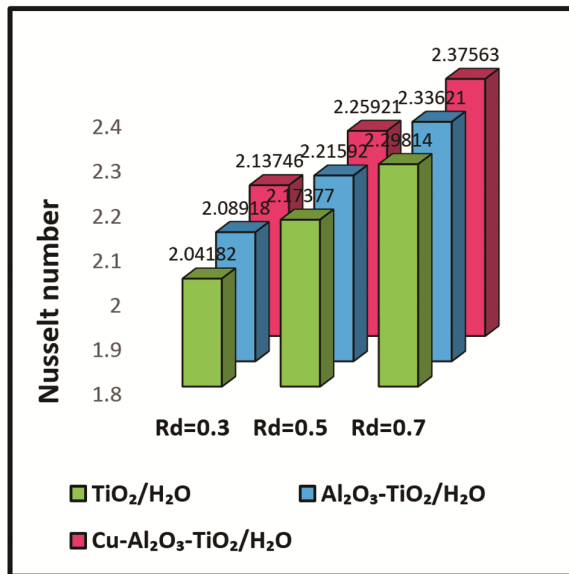


Fig. 10 — Discrepancy in Nusselt number against Rd

for the cases of $\text{Cu-TiO}_2/\text{H}_2\text{O}$, $\text{Cu-Al}_2\text{O}_3/\text{H}_2\text{O}$ hybrid nanofluid and $\text{Cu-Al}_2\text{O}_3\text{-TiO}_2/\text{H}_2\text{O}$ ternary nanofluid. The sway of Prandtl number Pr and thermal relaxation parameter δ_e on $Nu_x(\text{Re}_x)^{-0.5}$ is displayed in Fig. 8. It is visualised that the RHT intensifies for improved values of Pr and δ_e . Also, the trihybrid nanofluid

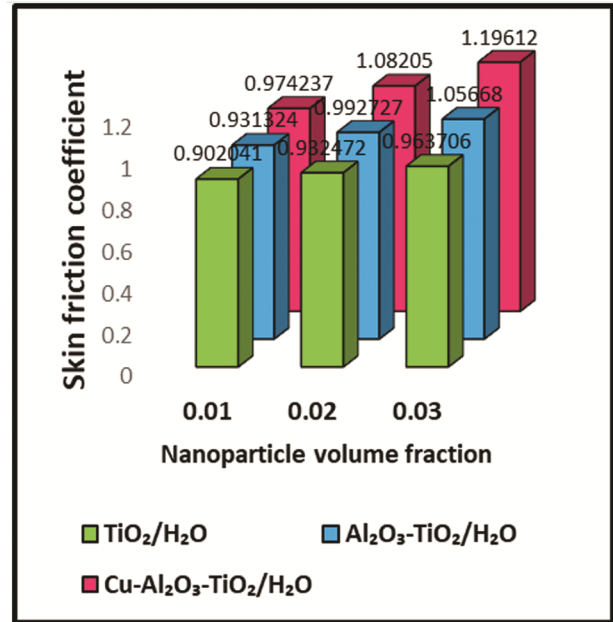


Fig. 11 — Skin friction analysis of ternary hybrid nanofluid based on $\phi_1, \phi_2,$ and ϕ_3

$\text{Cu-Al}_2\text{O}_3\text{-TiO}_2/\text{H}_2\text{O}$ appears to have significantly higher RHT than $\text{Cu-TiO}_2/\text{H}_2\text{O}$ and $\text{Cu-Al}_2\text{O}_3/\text{H}_2\text{O}$ hybrid nanofluid.

The influence of thermal relaxation parameter δ_e and radiation parameter Rd on the RHT for $\text{TiO}_2/\text{H}_2\text{O}$ nanofluid, $\text{Al}_2\text{O}_3\text{-TiO}_2/\text{H}_2\text{O}$ hybrid nanofluid and $\text{Cu-Al}_2\text{O}_3\text{-TiO}_2/\text{H}_2\text{O}$ ternary hybrid nanofluid are illustrated in Figs 9-10. The RHT for $\text{TiO}_2/\text{H}_2\text{O}$ nanofluid upsurges from 2.70597 to 2.74142 when δ_e varies between 0.05 and 0.2. During the same range of δ_e , $\text{Al}_2\text{O}_3\text{-TiO}_2/\text{H}_2\text{O}$ hybrid nanofluid and $\text{Cu-Al}_2\text{O}_3\text{-TiO}_2/\text{H}_2\text{O}$ ternary hybrid nanofluid exhibit thermal transmission rates ranging from 2.73652 to 2.768 and 2.76417 to 2.78989, respectively. Additionally, the ternary hybrid nanofluid demonstrated better rate of thermal transfer compared to $\text{TiO}_2/\text{H}_2\text{O}$ hybrid nanofluid by approximately 3.26-4.47 % for varying values of radiation parameter. Thus, augmenting the values of δ_e and Rd seems to have a positive impact on the thermal transfer rate.

Fig. 11-12 illustrate the variation in surface drag force and thermal transfer coefficient with a greater

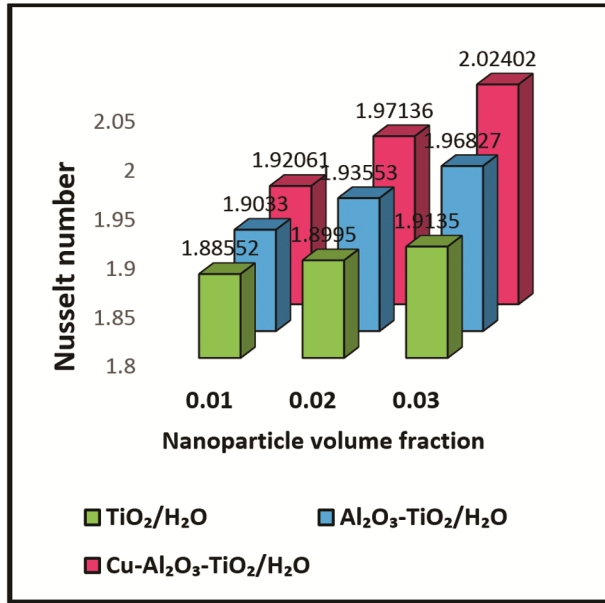


Fig. 12 — Nusselt number analysis of ternary hybrid nanofluid based on ϕ_1, ϕ_2 , and ϕ_3

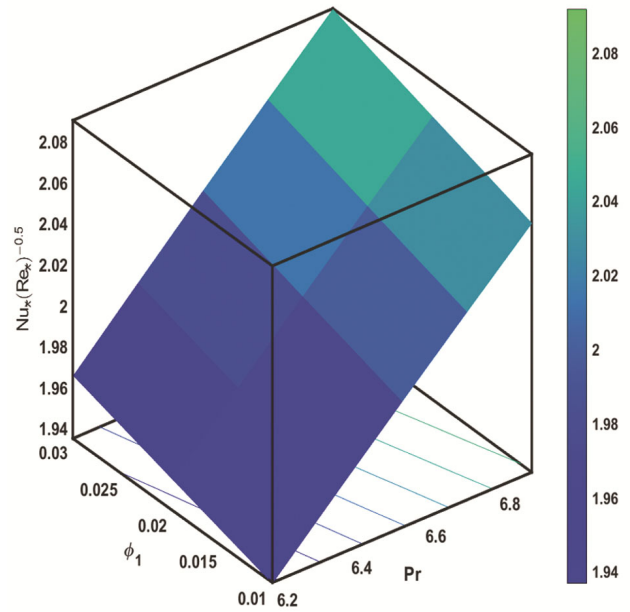


Fig. 14 — Implication of Pr and ϕ_1 on $Nu_{\bar{x}}(Re_{\bar{x}})^{-0.5}$

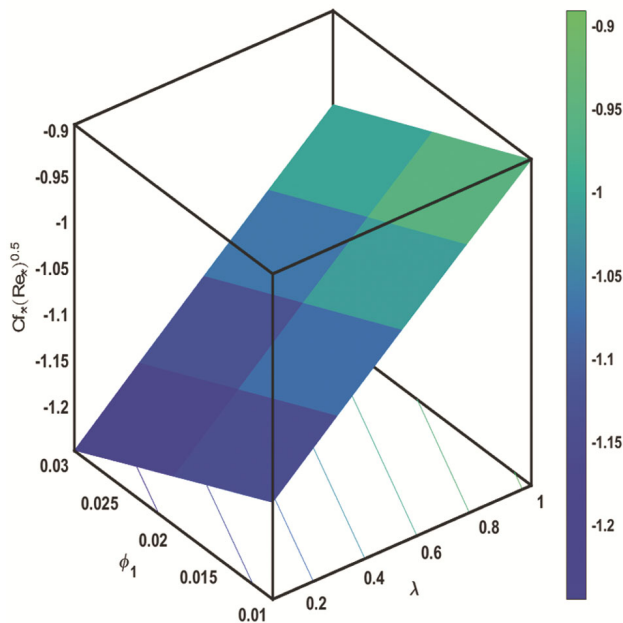


Fig. 13 — Implication of λ and ϕ_1 on $C_{f_{\bar{x}}}(Re_{\bar{x}})^{0.5}$

fraction of the nanoparticles, ϕ_1, ϕ_2 , and ϕ_3 . As a result of variations in ϕ_1, ϕ_2 , and ϕ_3 values between 0.01 and 0.03, the skin friction coefficients of TiO₂/H₂O nanofluid vary from 0.902041 to

0.963706 and for Al₂O₃-TiO₂/H₂O hybrid nanofluid, they range from 0.931324 to 1.05668 whereas for Cu-Al₂O₃-TiO₂/H₂O, the surface drag force vary between 0.974237 to 1.19612. It can be inferred from Fig. 12 that the thermal transfer of Cu-Al₂O₃-TiO₂/H₂O enhances by 1.83-5.46% approximately when compared to TiO₂/H₂O when ϕ_1, ϕ_2 , and ϕ_3 varies from 0.01 to 0.03. Thus, boosting the volume fraction accelerates the RHT of Cu-Al₂O₃-TiO₂/H₂O. The purpose of Fig. 13 is to examine how λ and ϕ_1 influence $C_{f_{\bar{x}}}(Re_{\bar{x}})^{0.5}$. Here $C_{f_{\bar{x}}}(Re_{\bar{x}})^{0.5}$ upsurges for higher λ while it diminishes for enhancing ϕ_1 values. Fig. 14 exhibits that $Nu_{\bar{x}}(Re_{\bar{x}})^{-0.5}$ gets positively influenced by the increasing Pr and ϕ_1 values. The performance of $Nu_{\bar{x}}(Re_{\bar{x}})^{-0.5}$ with reference to Rd and δ_e is depicted in Fig. 15. It is perceived that $Nu_{\bar{x}}(Re_{\bar{x}})^{-0.5}$ augments with both elevating Rd and δ_e values. The variation of the streamline patterns on the Cu-Al₂O₃-TiO₂/H₂O flow with respect to the

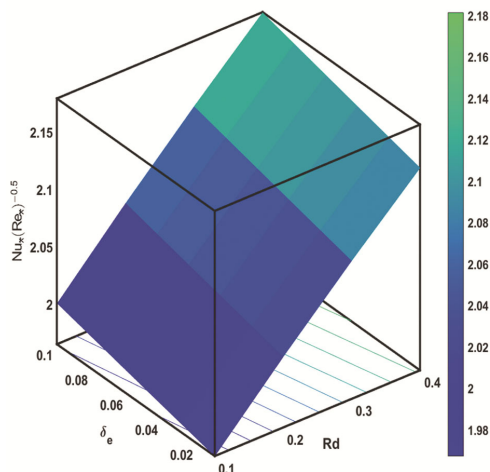


Fig. 15 — Implication of Rd and δ_e on $Nu_{\bar{x}}(Re_{\bar{x}})^{-0.5}$

mixed convection parameter λ is elucidated through Fig. 16(a-b). Essentially, a consistently augmented λ produces a considerable buoyant force resulting in more kinetic energy which in turn boosts the velocity profile of $Cu - Al_2O_3 - TiO_2 / H_2O$. The features of $Nu_{\bar{x}}(Re_{\bar{x}})^{-0.5}$ for various parameters are detailed in Table 3. The heat transmission coefficient $Nu_{\bar{x}}(Re_{\bar{x}})^{-0.5}$ enhances for increasing Rd , Pr and δ_e values.

Affirmation of results

The accuracy of the obtained results is evaluated in Table 4. The current results are validated for a special case of our work by those earlier reported results⁴²⁻⁴⁵. It is evident that there is an exceptional agreement between the outcomes.

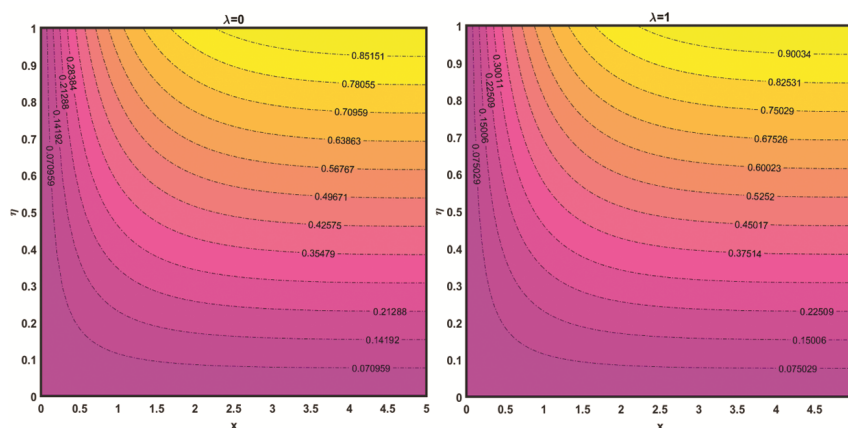


Fig.16 — Streamlines for $Cu - Al_2O_3 - TiO_2 / H_2O$ for (a) $\lambda = 0$ (b) $\lambda = 1$

Table 3 — Numerical results of $Nu_{\bar{x}}(Re_{\bar{x}})^{-0.5}$ with regard to distinct parameters

λ	Rd	Pr	δ_e	$Nu_{\bar{x}}(Re_{\bar{x}})^{-0.5}$
0.1	0.1	6.2	0.02	2.40945
		6.5		2.62314
		6.9		2.85482
0.1	0.4	6.2	0.02	3.10729
		6.5		3.19416
		6.9		3.30696
0.1	0.4	6.2	0.01	3.1013
		6.5	0.03	3.11331
		6.9	0.05	3.12544

Table 4 — Comparison of $-\theta'(0)$ with⁴²⁻⁴⁵ when $\phi_1 = \phi_2 = \phi_3 = Rd = \delta_e = \lambda = 0$

Pr	Ahmad <i>et al.</i> ⁴²	Khan <i>et al.</i> ⁴³	Shaiq <i>et al.</i> ⁴⁴	Devi and Devi ⁴⁵	Current results
2	0.9111	0.9119	0.9114	0.91135	0.9112395
6.13	1.7595	-	-	1.75968	1.7596364
7.0	1.8952	1.8994	1.8954	1.89540	1.8953462
20.0	3.3538	3.3533	3.3539	3.35390	3.3539254

Conclusion

The current study examines the mixed convective flow of a $Cu-Al_2O_3-TiO_2/H_2O$ ternary hybrid nanofluid past an elongated sheet with the application of C-C heat flux model. Additionally, the sway of heat radiation is also considered. By utilizing the similarity transformation, the equations governing the flow were transformed into dimensionless ODEs, which were followed by a numerical solution. The results listed below are some of the substantial conclusions made from this investigation:

- The augmentation of mixed convective parameter leads to an enhancement in the velocity profile.
- Increasing the radiation parameter enhances the temperature profile of the tri-hybrid nanofluid.
- The skin friction coefficient of $Cu-Al_2O_3-TiO_2/H_2O$ surpasses $Al_2O_3-TiO_2/H_2O$ approximately by 4.4-11.7% for varying volume fraction of the nanoparticles.
- An elevation in thermal relaxation parameter strongly boosts the rate of heat transfer.
- The tri-hybrid nanofluid $Cu-Al_2O_3-TiO_2/H_2O$ exhibits approximately 1.82-5.46% enhanced thermal transfer efficiency compared to TiO_2/H_2O for increasing values of volume fraction of the nanoparticle.

Nomenclature

(\tilde{u}, \tilde{v})	Velocity components along (\tilde{x}, \tilde{y}) axis	λ_r	Thermal relaxation time
g_r	acceleration due to gravity	δ_e	Thermal relaxation parameter
\tilde{T}	Nanofluid temperature	ϕ_1	Volume fraction of Cu nanoparticles
\tilde{T}_∞	Ambient temperature	ϕ_2	Volume fraction of Al_2O_3 nanoparticles
\tilde{T}_w	Wall temperature	ϕ_3	Volume fraction of TiO_2 nanoparticles
k^*	Mean absorption coefficient	η	Similarity variable
λ	Mixed convection or buoyancy parameter	θ	non-dimensional temperature
Rd	Radiation parameter	μ_f	Dynamic viscosity of the fluid
Pr	Prandtl number	ρ_f	Density of the fluid

$Gr_{\tilde{x}}$	Local Grashof number	$(\rho c_p)_f$	Heat capacity of the fluid
$Re_{\tilde{x}}$	Local Reynolds number	$(\rho \beta_T)_f$	Thermal expansion coefficient of the fluid
c_p	Specific heat at constant pressure	k	Thermal conductivity of the fluid
<i>Greek symbols</i>		<i>Subscripts</i>	
μ_{mf}	Viscosity of ternary nanofluid	f	fluid
ρ_{mf}	Density of ternary nanofluid	nf	nanofluid
$(\rho \beta_T)_{mf}$	Thermal expansion coefficient of ternary nanofluid	hmf	hybrid nanofluid
k_{mf}	Thermal conductivity of ternary nanofluid	tnf	ternary hybrid nanofluid
$(\rho c_p)_{mf}$	Heat capacity of ternary nanofluid	<i>Superscript</i>	
σ^*	Stefan-Boltzmann constant	' Differentiation with respect to η	

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